



# SNS COLLEGE OF ENGINEERING

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AN AUTONOMOUS INSTITUTION



Approved by AICTE, New Delhi and Affiliated to Anna University, Chennai

## DEPARTMENT OF ELECTRICAL AND ELECTRONICS ENGINEERING

### POWER SYSTEM ANALYSIS

#### UNIT - III

#### STEPPER MOTOR

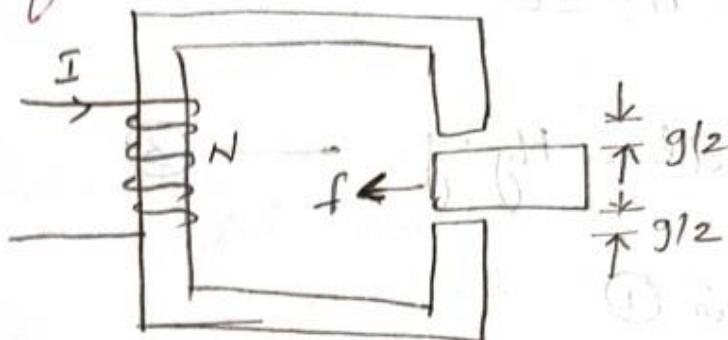
#### TORQUE EQUATION

Torque equation of Stepper Motor.

Basic assumptions.

- \* Internal magnetic energy & co-energy
- \* Considering ideal case of rotor & stator cores have infinite permeability.
- \* Proceed step by step to the case in which the cores are subject to magnetic saturation.

Infinite permeable core



Activate  
Go to Sett

A current  $I$ , is flowing through the coil of  $N$  turns to yield the magnetic flux, for  $f'$  is acting on iron piece in the  $x$ -direction.

Let  $B_g$  - magnetic flux density in the airgaps.

Amperes law.

$$\oint H \cdot dL = n I \quad \text{--- (1)}$$

$$\begin{aligned} \oint H \cdot dL &= H_g(g/2) + H_g(g/2) + H_i(l) \\ &= H_g(g) + H_i(l) \quad \text{--- (2)} \end{aligned}$$

where

$H_g$  = Magnetic field intensity in the gap.

$H_i$  = Magnetic field intensity in the cores.

$l$  - Total magnetic path in cores.

When permeability of cores is extremely large,  $\therefore H_i = 0$

$$\oint H \cdot dL = H_g \cdot g \quad \text{--- (3)}$$

Sub ③ in ①

$$Hg \cdot g = nI \quad \text{I passed A}$$
$$Hg = \frac{nI}{g} \longrightarrow ④$$

The air gap flux density

$$B_g = \frac{\mu_0 n I}{g} \longrightarrow ⑤$$

$\mu_0$  = Permeability in the air gap

Over lapped area =  $\pi a \omega$  — ⑥

where

$a$  = length of iron piece

$\omega$  = distance by which the rotor tooth & iron piece overlap.

Magnetic flux  $\phi = \text{area} \times B_g$

$$\phi = \pi a \omega \times \frac{\mu_0 n I}{g} \longrightarrow ⑦$$

Flux linkage  $\psi = n \phi$

$$\psi = \pi a \omega \frac{\mu_0 n^2 I}{g} \longrightarrow ⑧$$

Now, let us assume that there is an incremental displacement  $\Delta x$  of the tooth during a time interval  $\Delta t$ .

$$\Delta\psi = \frac{\omega \mu_0 n^2 I}{g} \Delta x \quad \textcircled{9}$$

The emf induced in the coil by the change in flux linkage is

$$e = -\frac{\Delta\psi}{\Delta t} = -\frac{\omega \mu_0 n^2 I}{g} \cdot \frac{\Delta x}{\Delta t} \quad \textcircled{10}$$

Work done by the source is

$$\Delta P_i = I |e| \Delta t$$

$$= \frac{\omega \mu_0 n^2 I^2}{g} \cdot \Delta x \quad \textcircled{11}$$

$$\Delta P_i = \frac{B g^2}{\mu_0} g \Delta x \quad \textcircled{12}$$

The work done by the source is converted partly to mechanical work & the rest spent in the magnetic field energy in airgaps.

$$\Delta \omega_m = \frac{1}{2} \frac{B_0^2}{\mu_0} g \omega \Delta x \quad \text{--- (13)}$$

h.c.T

$$\Delta \omega_m = f \Delta x$$

$$f \Delta x = \frac{1}{2} \frac{B_0^2}{\mu_0} g \omega \Delta x$$

$$f = \frac{1}{2} \frac{B_0^2}{\mu_0} g \omega$$

--- (14)

Sub eq (8) in (14)

$$f = \frac{1}{2} \frac{\omega \mu_0 n^2 I^2}{g}$$

--- (15)

$$W_m = \frac{1}{2} \frac{B_0^2}{\mu_0} g \omega \quad \text{--- (16)}$$

from eq (14) & (16)

$$f = \left( \frac{dW_m}{dx} \right)_I = \text{Constant.} \quad \text{--- (17)}$$

