## **INTEGRATOR**

If we interchange the resistor and capacitor of the differentiator of Fig. 4.21 (a), we have the circuit of Fig. 4.23 (a) which as we will see, is an integrator. The nodal equation at node N is,

$$\frac{v_i}{R_1} + C_f \frac{dv_o}{dt} = 0 \tag{4.77}$$

or,

$$\frac{dv_{o}}{dt} = -\frac{1}{R_{1}C_{f}}v_{i}$$

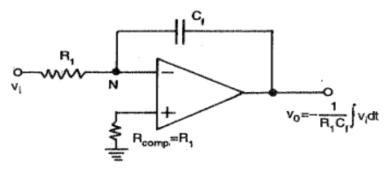


Fig. 4.23 (a) Op-amp integrator

Integrating both sides, we get,

$$\int_{0}^{t} dv_{0} = -\frac{1}{R_{1}C_{1}} \int_{0}^{t} v_{1} dt$$

## Practical Integrator Circuit (Lossy Integrator)

The gain of an integrator at low frequency (dc) can be limited to avoid the saturation problem if the feedback capacitor is shunted by a resistance  $R_{\rm f}$  as shown in Fig. 4.23 (c). The parallel combination of  $R_{\rm f}$  and  $C_{\rm f}$  behaves like a practical capacitor which dissipates power unlike an ideal capacitor. For this reason, this circuit is also called a lossy integrator. The resistor  $R_{\rm f}$  limits the low frequency gain to  $-R_{\rm f}/R_{\rm 1}$  (generally  $R_{\rm f}=10~R_{\rm 1}$ ) and thus provides dc stabilization.

## Analysis

The nodal equation at the inverting input terminal of the op-amp of Fig. 4.23 (c) is,

$$\frac{V_{\rm i}(s)}{R_1} + s C_{\rm f} V_{\rm o}(s) + \frac{V_{\rm o}(s)}{R_{\rm f}} = 0 \tag{4.82}$$

from which we have,

$$V_{0}(s) = -\frac{1}{sR_{1}C_{f} + R_{1}/R_{f}}V_{i}(s)$$
 (4.83)

If  $R_f$  is large, the lossy integrator approximates the ideal integrator. For  $s = j\omega$ , magnitude of the gain of lossy integrator is given by

$$|A| = \left| \frac{V_o}{V_i} \right| = \frac{1}{\sqrt{\omega^2 R_1^2 C_f^2 + R_1^2 / R_f^2}} = \frac{R_f / R_1}{\sqrt{1 + (\omega R_f C_f)^2}}$$
(4.84)

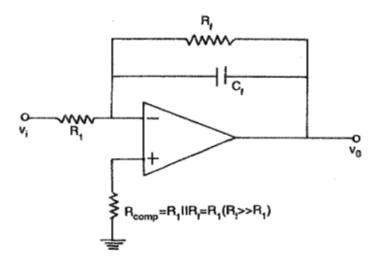


Fig. 4.23 (c) Practical or lossy integrator circuit

The Bode plot of the lossy integrator is also shown in Fig. 4.23 (b). At low frequencies gain is constant at  $R_f/R_1$ . The break frequency  $(f = f_a)$  at which the gain is 0.707  $(R_f/R_1)$  (or – 3dB below its value of  $R_f/R_1$ ) is calculated from Eq. (4.84) as

$$\sqrt{1 + (\omega R_{\rm f} C_{\rm f})^2} = \sqrt{2}$$

Solving for  $f = f_a$ , we get

$$f_{\rm a} = \frac{1}{2\pi R_{\rm f} C_{\rm f}}$$

This is a very important frequency. It tells us where the useful integration range starts. If the input frequency is lower than  $f_a$  the circuit acts like a simple inverting amplifier and no integration results. At input frequency equal to  $f_a$ , 50% accuracy results. The practical thumb rule is that if the input frequency is 10 times  $f_a$ , than 99% accuracy can result.